

## CHAPTER-9. CONTROL SYSTEM

[1] An open loop system represented by the transfer function  $G(s) = (s-1) / (s+2)(s+3)$  is

- A. stable and of the minimum phase type
- B. stable and of the non-minimum phase type**
- C. unstable and of the minimum phase type
- D. unstable and of the non-minimum phase type

[2] The open loop transfer function  $G(s)$  of a unity feedback control system is given as,

$$G(s) = [k(s+2/3) / s^2(s+2)]$$

From the root locus, it can be inferred that when  $k$  tends to positive infinity,

- A. three roots with nearly equal real parts exist on the left half of the s-plane**
- B. one real root is found on the right half of the s-plane
- C. the root loci cross the  $j\omega$  axis for a finite value of  $k$ ;  $k \neq 0$
- D. three real roots are found on the right half of the s-plane

[3] Given that

$$A = \begin{bmatrix} -5 & -3 \\ 2 & 0 \end{bmatrix} \text{ and } I = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix},$$

then the value of  $A^3$  is [GATE2012]

- A.  $15A+12I$
- B.  $19A+30I$**
- C.  $17A+15I$
- D.  $17A+21I$

[4] The matrix  $[A]=$

$$\begin{bmatrix} 2 & 1 \\ 4 & -1 \end{bmatrix}$$

is decomposed into a product of a lower triangular matrix  $[L]$  and an upper triangular matrix  $[U]$ . The properly decomposed  $[L]$  and  $[U]$  matrices respectively are.....The options A,B,C,D are given below.

$\begin{bmatrix} 1 & 0 \\ 4 & -1 \end{bmatrix}$ and $\begin{bmatrix} 1 & 1 \\ 0 & -2 \end{bmatrix}$	$\begin{bmatrix} 2 & 0 \\ 4 & -1 \end{bmatrix}$ and $\begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$	$\begin{bmatrix} 1 & 0 \\ 4 & 1 \end{bmatrix}$ and $\begin{bmatrix} 2 & 1 \\ 0 & -1 \end{bmatrix}$	$\begin{bmatrix} 2 & 0 \\ 4 & -3 \end{bmatrix}$ and $\begin{bmatrix} 1 & 0.5 \\ 0 & 1 \end{bmatrix}$
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A

B

C

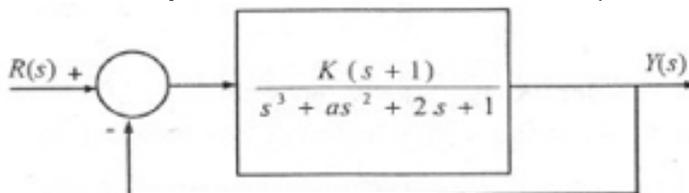
D

**Ans: none of the above**

[5] The input  $x(t)$  of a system are related as  $y(t) = \int_{-\infty}^t x(\tau) \cos(3\tau) d\tau$ . The system is [GATE2012]

- A. time-invariant and stable
- B. stable and not time-invariant**
- C. time-invariant and not stable
- D. not time-invariant and not stable

[6] The feedback system shown below oscillates at 2 rad/s when [GATE2012]



A.  $k=2$  and  $a=0.75$

B.  $k=3$  and  $a=0.75$

C.  $k=4$  and  $a=0.5$

D.  $k=2$  and  $a=0.5$

[7] The Fourier transform of a signal  $h(t)$  is  $H(j\omega) = (2\cos\omega)(\sin 2\omega)/\omega$ . The value of  $h(0)$  is [GATE2012]

A.  $1/4$

B.  $1/2$

C. 1

D. 2

[8] The state variable description of an LTI system is given by

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = \begin{pmatrix} 0 & a_1 & 0 \\ 0 & 0 & a_2 \\ a_3 & 0 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} u$$
$$y = (1 \ 0 \ 0) \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$

where  $y$  is the output and  $u$  is the input. The system is controllable for, [GATE2012]

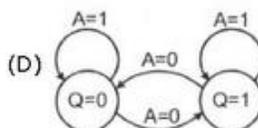
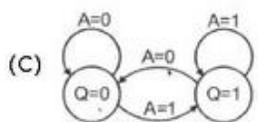
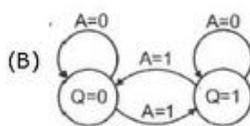
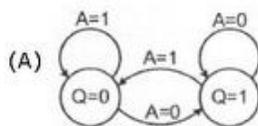
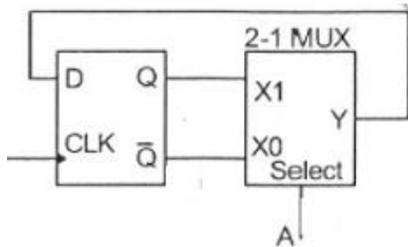
A.  $a_1 \neq 0, a_2 = 0, a_3 \neq 0$

B.  $a_1 = 0, a_2 = 0, a_3 \neq 0$

C.  $a_1 = 0, a_2 = 0, a_3 = 0$

D.  $a_1 \neq 0, a_2 \neq 0, a_3 = 0$

[9] The state transition diagram for the logic circuit shown is [GATE2012]



Ans: D

[10] Given that

$$A = \begin{bmatrix} -5 & -3 \\ 2 & 0 \end{bmatrix} \text{ and } I = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix},$$

then the value of  $A^3$  is [GATE2012]

A.  $15A+12I$

**B. 19A+30I**

**C. 17A+15I**

**D. 17A+21I**

[11] A system is described by the following state and output equations

$$[dx_1(t)/dt] = -3x_1(t) + x_2(t) + 2u(t)$$

$$[dx_2(t)/dt] = -2x_2(t) + u(t)$$

$$y(t) = x_1(t)$$

where  $u(t)$  is the input and  $y(t)$  is the output

The system transfer function is [GATE 2009]

**A.**  $(s+2)/(s^2+5s-6)$

**B.**  $(s+3)/(s^2+5s+6)$

**C.**  $(2s+5)/(s^2+5s+6)$

**D.**  $(2s-5)/(s^2+5s-6)$

**Ans: C**

[12] A two-port network is defined by the relation: [IES 2010]

$$I_1 = 5V_1 + 3V_2$$

$$I_2 = 2V_1 - 7V_2$$

The value of  $Z_{12}$  is

**A.** 3

**B.** -3

**C.** 3/41

**D.** 2/31

**Ans: C**

[13] The Z-transform of  $x(k)$  is given by [IES 2010]

$$x(Z) = \frac{\{(1-e^{-T})z^{-1}\}}{\{(1-z^{-1})(1-e^{-T}z^{-1})\}}$$

The initial value of  $x(0)$  is

**A.** Zero

**B.** 1

**C.** 2

**D.** 3

**Ans: A**

[14] Consider the following statements with reference to the phase plane:

1. They are general and applicable to a system of any order.
2. Steady state accuracy and existence of limit cycle can be predicted **D.**
3. Amplitude and frequency of limit cycle if exists can be evaluated **D.**
4. Can be applied to discontinuous time system.

Which of the above statements are correct? [IES2010]

**A.** 1,2,3 and 4

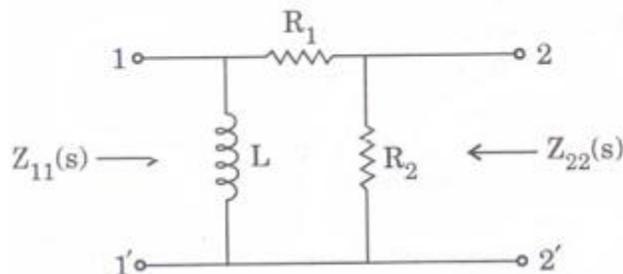
**B.** 2 and 3 only

**C.** 3 and 4 only

**D.** 2,3 and 4 only

**Ans: B**

[15] For the circuit shown below, the natural frequencies at port 2 are given by  $s+2=0$  and  $s+5=0$ , without knowing which refers to open-circuit and which to short-circuit. Then the impedances  $Z_{11}$  and  $Z_{22}$  are given respectively by [IES2010]



- A.  $K_1\{(s+5)/(s+2)\}, K_2\{(s+2)/(s+5)\}$
- B.  $K_1\{(s+2)/(s+5)\}, K_2\{(s+5)/(s+2)\}$
- C.  $K_1\{s/(s+2)\}, K_2\{(s+2)/(s+5)\}$
- D.  $K_1\{(s+2)/(s+5)\}, K_2\{(s+2)/(s+5)\}$

**Ans: C**

[16] Consider the following statements in connection with two-position controller:

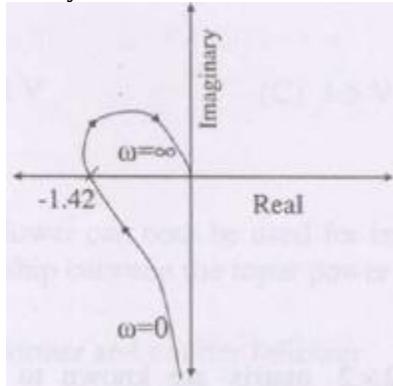
- 1.If the controller has a 4% neutral zone,its positive error band will be 2% and negative error band will be 8%.
- 2.The neutral zone is also known as dead band.
- 3.The controller action of a two-position controller is very similar to that of a pure on-off controller.
- 4.Air-conditioning system works essentially on a two-position control basis.

Which of the above statements are correct? [IES2010]

- A. 1,2 and 3 only.
- B. 2,3 and 4 only.
- C. 2 and 4 only.
- D. 1,2,3 and 4

**Ans:B**

[17] The polar plot of an open loop stable system is shown below. The closed loop system is [GATE 2009]



- A.Always stable
- B Marginally stable
- C.Unstable with one pole on the RH s-plane
- D.Unstable with two poles on the RH s-plane

**Ans:C**

[18] The open loop transfer function of a unity feedback system is given by  $G(s) = (e^{-0.1s})/s$ .The gain margin of this system is

[GATE 2009]

- A. 11.95 dB
- B. 17.67 dB
- C. 21.33 dB
- D. 23.9 dB

**Ans: D**

[19]The first two rows of Routh's tabulation of a third order equation are as follows.

$$s^3 \quad 2 \quad 2$$

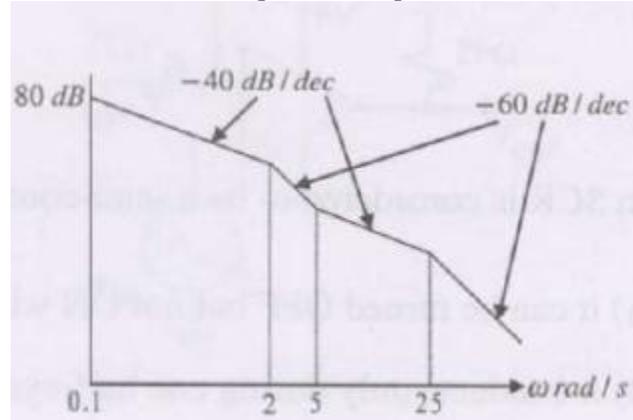
$$s^2 \quad 4 \quad 4$$

This means there are [GATE 2009]

- A. Two roots at  $s = \pm j$  and one root in right half s-plane
- B. Two roots at  $s = \pm j2$  and one root in left half s-plane
- C. Two roots at  $s = \pm j2$  and one root in right half s-plane
- D. Two roots at  $s = \pm j$  and one root in left half s-plane

**Ans:D**

[20]The asymptotic approximation of the log magnitude vs frequency plot of a system containing only real poles and zeros is shown. Its transfer function is [GATE 2009]



- A.  $[10(s+5)]/[s(s+2)(s+25)]$
- B.  $[1000(s+5)]/[s^2(s+2)(s+25)]$
- C.  $[100(s+5)]/[s(s+2)(s+25)]$
- D.  $[80(s+5)]/[s^2(s+2)(s+25)]$

**Ans:B**

[21]The trace and determinant of a 2x2 matrix are known to be -2 and -35 respectively. Its eigen values are [GATE 2009]

- A. -30 and -5
- B. -37 and -1
- C. -7 and 5
- D. 17.5 and -2

**Ans:C**

[22]A Linear Time Invariant system with an impulse response  $h(t)$  produces output  $y(t)$  when input  $x(t)$  is applied. When the input  $x(t-\tau)$  is applied to a system with impulse response  $h(t-\tau)$ , the output will be [GATE 2009]

- A.  $y(t)$
- B.  $y(2(t-\tau))$
- C.  $y(t-\tau)$
- D.  $y(t-2\tau)$

**Ans:D**

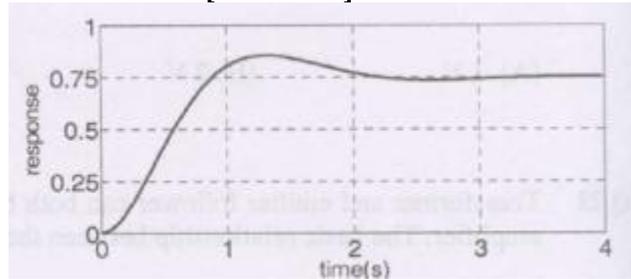
[23]For the Y-bus matrix of a 4-bus system given in per unit, the buses having shunt elements are [GATE 2009]

$$Y_{BUS} = j \begin{bmatrix} -5 & 2 & 2.5 & 0 \\ 2 & -10 & 2.5 & 4 \\ 2.5 & 2.5 & -9 & 4 \\ 0 & 4 & 4 & -8 \end{bmatrix}$$

- A. 3 and 4
- B. 2 and 3
- C. 1 and 2
- D. 1,2 and 4

**Ans: C**

[24] The unit step response of a unity feedback system with open loop transfer function  $G(s) = K / ((s+1)(s+2))$  is shown in the figure. The value of K is [GATE 2009]



- A. 0.5
- B. 2
- C. 4
- D. 6

**Ans: D**

[25] For the driving point impedance function,  $Z(s) = [as^2 + 7s + 3] / [s^2 + 3s + b]$ , the circuit realization is shown below. The values of 'a' and 'b' respectively are [IES2010]

- A. 4 and 5
- B. 2 and 5
- C. 2 and 1
- D. 2 and 3

**Ans: C**

[26] For the following driving point impedance functions, which of the following statements is true? [IES2010]

$$Z_1(s) = (s+2) / (s^2 + 3s + 5)$$

$$Z_2(s) = (s+2) / (s^2 + 5)$$

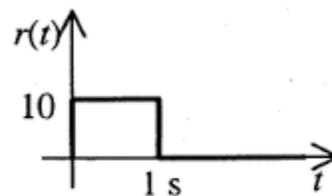
$$Z_3(s) = (s+2) / (s^2 + 2s + 1)$$

$$Z_4(s) = (s+2)(s+4) / (s+1)(s+3)$$

- A.  $Z_1$  is not positive real
- B.  $Z_1$  is positive real
- C.  $Z_3$  is positive real
- D.  $Z_4$  is positive real

**Ans: D**

[27] The steady state error of a unity feedback linear system for a unit step input is 0.1. The steady state error of the same system, for a pulse input  $r(t)$  having a magnitude of 10 and a duration of one second, as shown in the figure is [GATE2011]

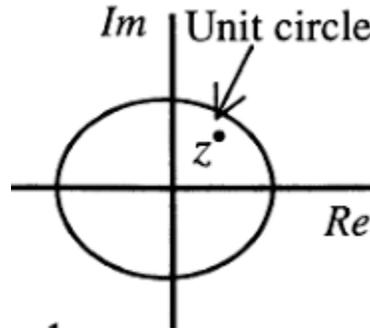


- A. 0
- B. 0.1
- C. 1

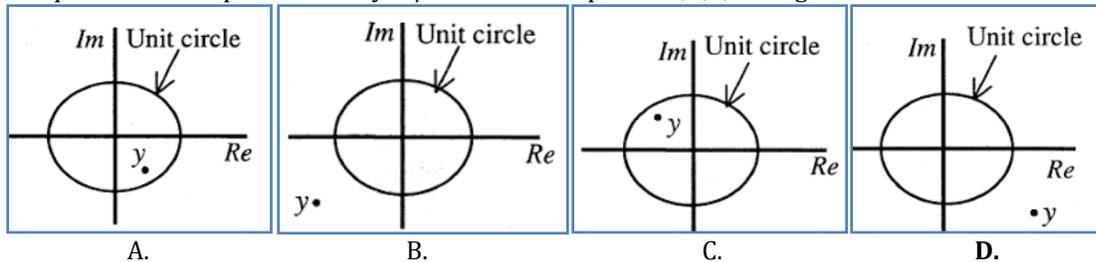
D. 10

Ans:A

[28] A point  $z$  has been plotted in the complex plane, as shown in figure below [GATE2011]



The plot of the complex number  $y=1/z$  is.....The options A,B,C,D are given below.



Ans:D

[29] The system represented by the input-output relationship  $y(t) = \int_{-\infty}^{5t} x(\tau) d\tau$ ,  $t > 0$  is

- A. Linear and casual
- B. Linear but not casual**
- C. Casual but not linear
- D. Neither linear nor casual

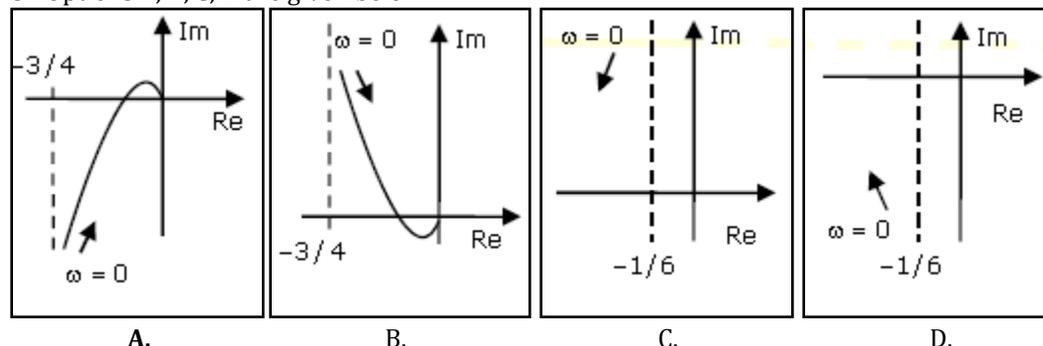
[30] For the system  $2/(s+1)$ , the approximate time taken for a step response to reach 98% of its final value is

- A. 1s
- B. 2s
- C. 4s**
- D. 8s

[33] Given the finite length input  $x[n]$  and the corresponding finite length output  $y[n]$  of an LTI system as shown below, the impulse response  $h[n]$  of the system is

- A.  $h[n] = \{1, 0, 0, 1\}$
- B.  $h[n] = \{1, 0, 1\}$
- C.  $h[n] = \{1, 1, 1, 1\}$**
- D.  $h[n] = \{1, 1, 1\}$

[34] The frequency response of  $G(s) = 1/[s(s+1)(s+2)]$  plotted in the complex  $G(j\omega)$  plane (for  $0 < \omega < \infty$ ) is....Options A, B, C, D are given below



Ans:A

[35] The system  $x=Ax+Bu$  with

A=

$$\begin{bmatrix} -1 & 2 \\ 0 & 2 \end{bmatrix}$$

B=

$$\begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

is

- A. stable and controllable
- B. stable but uncontrollable
- C. unstable but controllable**
- D. unstable and uncontrollable

[36] The characteristic equation of a closed-loop system is  $a(s+1)(s+3)+k(s+2)=0, k>0$ . Which of the following statements is true?

- A. Its roots are always real
- B. It cannot have a breakaway point in the range  $-1 < \text{Re}[s] < 0$
- C. Two of its roots tend to infinity along the asymptotes  $\text{Re}[s]=-1$**
- D. It may have complex roots in the right half plane

[37] The frequency response of a linear system  $G(j\omega)$  is provided in the tabular form below

$ G(j\omega) $	1.3	1.2	1.0	0.8	0.5	0.3
$\angle G(j\omega)$	$-130^\circ$	$-140^\circ$	$-150^\circ$	$-160^\circ$	$-180^\circ$	$-200^\circ$

- A. 6dB and  $30^\circ$**
- B. 6dB and  $-30^\circ$
- C. -6dB and  $30^\circ$
- D. -6dB and  $-30^\circ$

[38] An openloop system represented by the transfer function  $G(s) = \frac{s+1}{(s+2)(s+3)}$  is

- A. stable and of the minimum phase type
- B. stable and of the non-minimum phase type
- C. unstable and of the minimum phase type
- D. stable and of the non-minimum phase type**

[39] The open loop transfer function  $G(s)$  of a unity feedback control system is given as,  $G(s) = \frac{k(s+2/3)}{s^2(s+2)}$  From the root locus, it can be inferred that when  $k$  tends to positive infinity.

- A. three roots with nearly equal real parts exist on the left half of the s-plane**
- B. one real root is found on the right half of the s-plane
- C. the root loci cross the  $j\omega$  axis for a finite value of  $k$ ;  $k$  not equal to 0
- D. three real roots are found on the right half of the s-plane

[40] The response  $h(t)$  of a linear time invariant system to an impulse  $\delta(t)$ , under initially relaxed condition is  $h(t) = e^{-t} + e^{-2t}$ . The response of this system for a unit step input  $u(t)$  is

- A.  $u(t) + e^{-t} + e^{-2t}$
- B.  $(e^{-t} + e^{-2t}) u(t)$
- C.  $(1.5e^{-t} - 0.5e^{-2t}) u(t)$**
- D.  $e^{-t}\delta(t) + e^{-2t}u(t)$